On the interpretation of local models in blended multiple model structures

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The construction of non-linear dynamics by means of interpolating the behaviour of locally valid models offers an attractive and intuitively pleasing method of modelling non-linear systems. The approach is used in fuzzy logic modelling, operating regime based models, and non-linear statistical models. The model structure suggests that the composite local models can be used to interpret, in some appropriate manner, the overall non-linear dynamics. In this paper we demonstrate that the interpretation of these local models, in the context of multiple model structures, is not as straightforward as it might initially appear. We argue that the blended multiple model system can be interpreted in two ways—as an interpolation of linearizations, or as a full parameterization of the system. The choice of interpretation affects experiment design, parameter identification, and model validation. We then show that, in some cases, the local models give insight into full model behaviour only in a very small region of state space. More alarmingly, we demonstrate that for off-equilibrium behaviour, subject to some approximation error, a non-unique parameterization of the model dynamics exists. Hence, qualitative conclusions drawn from the behaviour of an identified local model, e.g. regarding stable, unstable, nodal or complex behaviour, must be treated with extreme caution. The example of muscle modelling is used to illustrate these points clearly.

1. Introduction

The past few years have shown an increase in the use of *local model representations* of non-linear dynamic systems (see Johansen and Murray-Smith 1997 for a review). This basic structure includes a number of approaches: *Tagaki-Sugeno* fuzzy systems (Takagi and Sugeno 1985), local model networks, gain-scheduled control, statistical mixture models, *Smooth Threshold AutoRegressive* (*STAR*) models of Tong (1990) and the *State dependent models* of Priestley (1988), among them. The model parameters are obtained from prior knowledge, linearizations of a physical model or identified from measured data. Advantages of this approach are purported to be its simplicity and the insight into global dynamics obtained from the local models.

By a blended local model structure we understand a dynamic model of the form

$$\dot{\mathbf{x}} = \sum_{i}^{N_m} \rho_i(\mathbf{x}, \mathbf{u}, \mathbf{w}) \mathbf{f}_i(\mathbf{x}, \mathbf{u})$$
(1.1)

where state $\mathbf{x} \in \mathbb{R}^N$, input $\mathbf{u} \in \mathbb{R}^P$, and an external vector $\mathbf{w} \in \mathbb{R}^O$, the model $\mathbf{f}_i(:,:)$ is one of N_m vector functions of the state and the input, and is valid in a region defined by the scalar validity function ρ_i , which in turn is a function of the above variables. Typically, the local

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models \mathbf{f}_i are chosen to be of the form $\mathbf{f}_i(\mathbf{x}, \mathbf{u}) = \mathbf{A}_i \mathbf{x} + \mathbf{B}_i \mathbf{u} + \mathbf{d}_i$, resulting in constituent dynamic systems Σ_i given by

$$\Sigma_{i} : \dot{\mathbf{x}} = \mathbf{f}_{i}(\mathbf{x}, \mathbf{u}) \tag{1.2}$$

$$= \mathbf{A}_i \mathbf{x} + \mathbf{B}_i \mathbf{u} + \mathbf{d}_i \qquad (1.3)$$

where $\mathbf{x}, \mathbf{d}_i \in \mathbb{R}^N$, $\mathbf{A}_i \in \mathbb{R}^{N \times N}$, and $\mathbf{B}_i \in \mathbb{R}^{N \times P}$. This results in a non-linear description of plant dynamics of the form

$$\dot{\mathbf{x}} = \mathbf{A}(\mathbf{x}, \mathbf{u}, \mathbf{w})\mathbf{x} + \mathbf{B}(\mathbf{x}, \mathbf{u}, \mathbf{w})\mathbf{u} + \mathbf{d}(\mathbf{x}, \mathbf{u}, \mathbf{w})$$
(1.4)

where

$$\mathbf{A}(\mathbf{x}, \mathbf{u}, \mathbf{w}) = \sum_{i}^{N_{m}} \rho_{i}(\mathbf{x}, \mathbf{u}, \mathbf{w}) \mathbf{A}_{i}$$
(1.5)

$$\mathbf{B}(\mathbf{x}, \mathbf{u}, \mathbf{w}) = \sum_{i}^{N_{m}} \rho_{i}(\mathbf{x}, \mathbf{u}, \mathbf{w}) \mathbf{B}_{i}$$
(1.6)

$$\mathbf{d}(\mathbf{x}, \mathbf{u}, \mathbf{w}) = \sum_{i}^{N_m} \rho_i(\mathbf{x}, \mathbf{u}, \mathbf{w}) \mathbf{d}_i$$
(1.7)

The \mathbf{A}_i matrices associated with each of the local models are assumed to be invertible; that is, associated with each constituent local model there is exactly one unique equilibrium point. Model building thus consists of covering the state space of the non-linear plant with local models. Behaviour along the plant equilibria is typically captured by using models whose equilibria $(\mathbf{x}_{i0} = -\mathbf{A}_i^{-1}\mathbf{d}_i)$, in the unforced case) are located inside the region defined by their basis functions, whereas behaviour off equilibria is captured by using models whose (virtual) equilibria are located outside the region defined by their basis functions (hence the 'virtual' label).

In this paper we demonstrate that the interpretation of local models is not straightforward, and depends both

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2. Interpretation and identification

Typically, identification of a local model network either involves conventional linearization of the nonlinear system about a number of equilibrium operating points, or performing weighted regression of local models to excitation data (in which case the models are not the classical linearizations commonly used in control theory).

Given these two possibilities, there are two approaches to interpretation of the model at intermediate operating points, where the model description of the plant dynamics is obtained by interpolating the local models in some manner. For example, consider the model of the unforced plant dynamics obtained by identifying linear models about several values of scheduling vector $(\mathbf{x}_i, \mathbf{w}_{0i})$:

- (1) We could interpret the interpolation procedure as yielding intermediate Jacobian matrices given by $\mathbf{A}(\mathbf{x}_0, \mathbf{w}_0)$. This results in a model of the linearized dynamics at $(\mathbf{x}_0, \mathbf{w}_0)$ given by $\dot{\mathbf{x}} =$ $\mathbf{A}(\mathbf{x}_0, \mathbf{w}_0)(\mathbf{x} - \mathbf{x}_0)$.
- (2) Or, we could assume that the multiple model family used *is* a parameterization of the real system yielding a full description of global dynamics $\dot{\mathbf{x}} = \mathbf{A}(\mathbf{x}, \mathbf{w})\mathbf{x} + \mathbf{d}(\mathbf{x}, \mathbf{w})$. In this case the linearization about an intermediate equilibrium point $(\mathbf{x}_0, \mathbf{w}_0)$ is given by

$$\dot{\mathbf{x}} = \left(\frac{\partial}{\partial x} [\mathbf{A}(\mathbf{x}, \mathbf{w})\mathbf{x} + \mathbf{d}(\mathbf{x}, \mathbf{w})]\right)_{(\mathbf{x}_0, \mathbf{w}_0)} (\mathbf{x} - \mathbf{x}_0) + \left(\frac{\partial}{\partial w} [\mathbf{A}(\mathbf{x}, \mathbf{w})\mathbf{x} + \mathbf{d}(\mathbf{x}, \mathbf{w})]\right)_{(\mathbf{x}_0, \mathbf{w}_0)} (\mathbf{w} - \mathbf{w}_0) \quad (2.1)$$

$$= \overline{\mathbf{A}}_{\mathbf{x}}(\mathbf{x}_0, \mathbf{w}_0) (\mathbf{x} - \mathbf{x}_0) + \overline{\mathbf{A}}_{\mathbf{w}}(\mathbf{x}_0, \mathbf{w}_0) (\mathbf{w} - \mathbf{w}_0)$$
(2.2)

where
$$\overline{\mathbf{A}}_{\mathbf{x}}(\mathbf{x}_0, \mathbf{w}_0) \in \mathbb{R}^{N \times N}$$
 and where $\overline{\mathbf{A}}_{\mathbf{w}}^{-}(\mathbf{x}_0, \mathbf{w}_0) \in \mathbb{R}^{N \times O}$.

(Note here we have omitted \mathbf{u} from the scheduling variable for simplicity. In the remainder of the paper we shall no longer schedule on an external \mathbf{w} and shall therefore use \mathbf{A} for $\mathbf{A}_{\mathbf{x}}$.)

If identifying the models from experimental data, the first interpretation implies that the linearization is based only on perturbation data around the linearization point $(\mathbf{x}_0, \mathbf{w}_0)$. In the second case [equation (2.1)], we assume global excitation of the input space, and that the local models are *not* to be identified independently of each other, but rather that the identification of basis functions and local models is performed in an iterative process. We note that $\overline{\mathbf{A}}_{\mathbf{x}}(\mathbf{x}_0, \mathbf{w}_0)$ and $\mathbf{A}(\mathbf{x}_0, \mathbf{w}_0)$ are in

general not identical. To sum up—what the model represents depends on how the data are gathered, and how the parameters of the local models and basis functions are identified.

Example 1: To illustrate this point more clearly, consider the example depicted in figure 1. Here, a mathematical model of a helicopter was perturbed (helicopter linearization data provided by Stewart Houston, University of Glasgow; the model is too extensive to include in this paper—see Houston (1994) for further details) around a number of linearization points x_i (scheduling on airspeed, from hover to 10 knots at 1 knot intervals) to provide the parameters for local state-space models, which are then integrated into a multiple model system using locally linear basis functions to form a model of the system dynamics. The use of perturbations around an operating point implies that we are using the first interpretation.

In figure 1 we show the eigenvalues of the $A(x_0)$ and $\overline{\mathbf{A}}(\mathbf{x}_0)$ matrices as defined above. Figure 1(c) shows the linearly interpolating basis functions, and their derivatives. In the second approach the non-zero derivatives of the basis functions, and of the offset terms have a significant effect on the linearizations. In figure 1(a) we see the poles of the identified A matrices, and interpolation between them provides 'sensible' results. These A matrices already implicitly contain the extra terms described in the second interpretation. If we interpret them wrongly by adding in the effect of basis function derivatives and change of offset, we get meaningless interpolation, as shown in figure 1(b), where the full model eigenvalues do not even pass through the local model eigenvalues at the linearization points (because of the non-zero derivative of the basis function, $\partial \rho_i(\mathbf{x}) / \partial \mathbf{x}$). Adding further local models would not improve matters.

This example illustrates the care which should be taken when interpreting the parameters of a multiple model system. (Note that one could argue for a variety of implementations of the basis function and local models for this case—the example is purely to illustrate the relevance of the points discussed above.) This obviously has to be taken into account when dealing with grey-box models which combine identified and *a priori* components, as well as for experiment design, identification algorithms and any subsequent control design.

3. Interpretation of model dynamics

The structure of the non-linear system (1.4) and the manner in which it is identified encourage a certain interpretation of the model dynamics; namely to interpret the model dynamics in terms of the individual dynamic systems Σ_i . In fact, the structure is such that it is quite



(a) Eigenvalues of $A(x_0)$ are marked by dots. Eigenvalues of linearizations A_i are circles.



(b) Eigenvalues of $\overline{\mathbf{A}}(\mathbf{x}_0)$ are marked by dots. Eigenvalues of linearizations \mathbf{A}_i are marked by circles. Note the divergence from the interpolated eigenvalues in (a), and that the interpolated eigenvalues no longer pass through the identified eigenvalues, even at the linearization points.

tempting to interpret the quantitative behaviour of the model dynamics in terms of the poles and zeros of Σ_i . Such an interpretation is not generally valid for a number of reasons. A part from the fact that the eigenvalues of the parameterized matrix A(x, u, w) depend not only on the local models A_i , B_i , d_i , but also upon the interpolation procedure, several other problems exist which invalidate this interpretation. In particular we note the following important observations which provide the basis for the remaining discussion in this paper.

(1) Local models along the manifold of equilibria are only individually interpretable in a region where $\rho_i \approx 1$. (For the second interpretation [equation (2.1)], we see that $\overline{A}_{\mathbf{x}_i}(\mathbf{x}) \approx \mathbf{A}_i$ only if $\rho_i \approx 1$ and $\partial \rho_i(\mathbf{x}) / \partial \mathbf{x} \approx 0$. Hence, the effect of



(c) Linear interpolation basis functions of local model net, and their derivatives. Basis functions have compact support. Basis functions are plotted for the region used for the interpolation plots in (a) and (b). The x-axis is normalized, with hover from the left to 10 knots on the right.

Figure 1. Illustration of the effect of model interpretation in a practical example. The local models were linearizations based on perturbations of a helicopter model from a trimmed stated, at 1 knot intervals from hover to 10 knots. Eigenvalues of individual local models are shown, along with interpolated values from the multiple model structure.

> the derivative may contribute significantly to the linearization term unless the neighbouring A_i s are identical.)

(2) Off equilibria, for models with virtual equilibrium points, only part of the dynamics associated with model Σ_i is used in the construction of the global dynamics. Hence, the region of validity of the model is more restricted than that defined by its blending function ρ_i . The model is only valid in a subspace of this region.

Both of these observations, and their consequences for interpreting structures such as the local model network (Johansen and Murray-Smith 1997) will now be discussed.

3.1. Interpretation problems of on-equilibrium local models

It is well known that instability and even chaotic behaviour can be introduced by switching or interpolating between *stable* linear systems (Fillipov 1960, Skoog and Clifford 1972, Shorten 1996). Hence, the dynamics of the individual sub-systems may, in some cases, give no useful insight into the global system dynamics. In the case of equation (1.4) such effects depend upon the validity functions and linearization points (hence the



(a) Model construction.

(b) Alternative model construction.

Figure 2. Construction of a trajectory using interpolated local models. The ellipses denote the location of the ρ_i . Note how alternative models' trajectories approximate the measured trajectory within their basis functions, but diverge significantly outside the basis function. This observation has severe consequences for control law design.

 \mathbf{d}_i)— the local linearizations are often only indicative of global dynamics in a small region where $\rho_i \approx 1$, around their equilibrium points. In this region, the global model behaves approximately as the local model, and returns to the equilibrium point. However, if perturbed such that the state leaves this region of the local model's operating regime, we may see periodic oscillatory behaviour, or chattering between neighbouring local models, and the state may even subsequently leave the local model's nodel's regime entirely, thereby rendering isolated interpretation of each local model meaningless.

3.2. Interpretation problems of off-equilibrium local models

A further factor which affects our interpretation of multiple model dynamics concerns off-equilibrium behaviour. Consider the phase-plane trajectory depicted in figure 2. It can be observed that the trajectory depicted may be approximated by combining models as shown in figure 2(a) or as in figure 2(b). This suggests that the state space can be covered by many different locally accurate models which, when combined, will approximate this trajectory in a satisfactory manner. To see this more clearly consider the abstract case of approximating the flow associated with the dynamic system $\dot{\mathbf{x}} = \mathbf{f}(\mathbf{x})$, in the vicinity of some vector \mathbf{x}_0 by the local model

$$\dot{\mathbf{x}} = \rho(\mathbf{x}) \left[\mathbf{A} \, \mathbf{x} + \, \mathbf{d} \right] \tag{3.1}$$

where $\mathbf{f}(:) \in \mathbb{R}^N$, where $\mathbf{x}, \mathbf{A}, \mathbf{d}$ are as defined in §1, and where $\rho(\mathbf{x}) = 1$ when $\mathbf{x} = \mathbf{x}_0$, and is zero otherwise. Clearly for any arbitrary choice of invertible \mathbf{A} , regardless of its nature (stable, unstable, complex, etc.), a vector \mathbf{d} can be found such that

$$\mathbf{f}(x_0) = \rho(\mathbf{x}_0) [\mathbf{A} \mathbf{x}_0 + \mathbf{d}]$$
(3.2)

where $\mathbf{d} = \mathbf{f}(\mathbf{x}_0) - \mathbf{A}\mathbf{x}_0$. Hence, at $\mathbf{x} = \mathbf{x}_0$ a non-unique parameterization of the dynamics exist, making any qualitative interpretation of the **A** matrix meaningless. Furthermore, in the neighbourhood of \mathbf{x}_0 , subject to some approximation error, by simply varying the location of the virtual equilibria (or of the form of the ρ_i), it is possible to obtain many (dynamically) different parameterizations of the non-linear dynamics. (We note also that conditions exist such that two systems, which have the same equilibrium point, can be identical along an entire manifold; namely, when \mathbf{A}_1 and \mathbf{A}_2 share eigenvector and eigenvalue pairs. The manifold is defined by the eigenvectors common to both systems.) This is illustrated in the following example.

Example 2: Consider the behaviour of the following autonomous systems

$$\boldsymbol{\Sigma}_1 : \dot{\mathbf{x}} = \mathbf{A}_1 \mathbf{x} \tag{3.3}$$

$$\Sigma_2 : \dot{\mathbf{x}} = \mathbf{A}_2 \mathbf{x} + \mathbf{d} \tag{3.4}$$

where

$$\mathbf{A}_{1} = \begin{bmatrix} 4 & -4.5 \\ 4.05 & -4.55 \end{bmatrix} \quad \mathbf{A}_{2} = \begin{bmatrix} 0.51 & -4.29 \\ 3.84 & -4.51 \end{bmatrix}$$

and

$$\mathbf{d} = \begin{bmatrix} -8.58\\ -0.27 \end{bmatrix}$$

The flow associated with both of these systems is depicted in figure 3. These systems are qualitatively very different; Σ_1 is a *stable node* with an equilibrium point centred at the origin, whereas Σ_2 is a *stable spiral*



Figure 3. Non-uniqueness of representation. The two systems Σ_1 and Σ_2 are qualitatively different, but in the outlined regions [shown in detail in (c) and (d)] we see that there is little difference, as shown by the error dynamics in (e).

with its equilibrium point close to, but not centred, at the origin. However, in a small region defined by

$$R: 2 \le x_1 \le 4, \qquad 8 \le x_2 \le 10 \tag{3.5}$$

as depicted, the flow of both systems is similar. The velocity vectors point in the same direction and the maximum error, defined by

$$\varepsilon_{\max} = \max_{x \in R} \frac{\| (\mathbf{A}_2 - \mathbf{A}_1) \mathbf{x} + \mathbf{d} \|}{\| \mathbf{x} \|}$$
(3.6)

$$< 0.42$$
 (3.7)

is bounded and small. The error dynamics

$$\dot{\mathbf{x}} = (\mathbf{A}_2 - \mathbf{A}_1)\mathbf{x} + \mathbf{d}, \qquad \mathbf{x} \in \mathbf{R}$$
(3.8)

are depicted in figure 3(e). Hence, we conclude that in R, subject to some appropriately defined approximation error, the dynamics described by Σ_{A_1} and Σ_{A_2} are in some sense equivalent. In this region both Σ_{A_1} and Σ_{A_2} are valid representations of an appropriate non-linear

system, but outside the region they differ considerably.

This rather obvious observation is of crucial importance for two reasons. It strongly suggests that the qualitative nature of the identified local models may say very little about the non-linear dynamics even locally. This is by virtue of the fact that the local model is, by definition, only valid in a local region of state space, and crucially in the off-equilibrium case, that the local model's contribution to the global model only comes from a restricted sub-region which does not include the model's equilibrium point. Given enough data, from a well-designed experiment, we could avoid such problems, as we would know we had covered the volume of interest in the input space. In practice though, where we have too poor understanding of the target system to design an ideal experiment, and where exhaustive data acquisition is too expensive, this will often be a real problem.



(a) Model behaviour over time. The responses of the unstable and of the modified model are almost identical.

(b) Phase plane trajectories of the unstable and the modified model shown in (a) from 150 to 300 ms. Bold line indicates that the fourth local model is active ($\rho_4 > 0.3$). The sudden vertical jumps in x are due to the input pulses shown in (a).

Figure 4. Experimental data and model responses.

Secondly, given the variability in possible solutions to the identification problem, we may wish to regularize the identification process, that is bias the choice from the space of possible fits to the data towards models with desired properties (for example stable local linear models). A simple alternative, especially if we only want onequilibrium models, so it is known a priori that local models should have 'real' equilibria, is to identify offset models $\mathbf{d}_i(\cdot)$ separately from dynamics models. This is a practical approach, as a wide class of systems can be easily driven through a range of equilibria to acquire the necessary data, and at a finer quantization level than in experiments linked to the dynamic behaviour. Straightforward interpolation with smoothing provides the model, and validation is also straightforward. If we then use this model of the offsets as the basis for the linearizations we have severely reduced the degrees of freedom for the linear system.

4. Modelling muscle behaviour

An example of identifying a local model with a virtual equilibrium point, and being able to correct problems (in this case 'by hand'), was found when modelling isometric contraction of electrically stimulated rabbit muscle (Gollee *et al.* 1997). The motoneurons of the muscle are stimulated with randomly spaced impulses, and the force produced by the muscle when held at constant length is recorded. Typical data are shown in figure 4(a). The system has a single input and a single output.

A model of the form of equation (1.4) with six local linear second order models is identified using 30 data sets, where each set contains 590 samples. The parameters of the local models were optimized using a Levenberg-Marquardt algorithm with an infinite prediction horizon (Press *et al.* 1992). As shown in figure 4(a), the performance of the global model is very good for stimulation sequences similar to those used to identify its parameters, which consist of pulses with randomly varying inter-pulse interval. If we examine the identified A matrices, we find that all have real and negative eigenvalues, except for the fourth local model which has eigenvalues 7.14, - 111.89, i.e. this local model has a non-stable A matrix, which is undesirable-if the model enters a region where we had no identification data, a stable matrix will tend to push us toward equilibria and thus hopefully into a more accurately modelled region. (It could also lead to limit cycle behaviour, but should not lead to unboundedness.) All local models, other than the one scheduled at w = 0 have virtual equilibria. Given the stimulation the model was identified with, where the activation varies quickly, and each local model remains activated only for a short period of time, this slow positive eigenvalue did not have time to have an effect. However, the influence of the unstable

0.8



(a) Responses of the full models to constant frequency burst of 37 Hz (stimulation and scheduling variables shown in the upper plot)



Figure 5. Responses of the gobal models, and phase planes and state trajectories of the unstable and the stable local model for an input stimulation with a constant pulse frequency of 37 Hz. The vertical jumps in the phase plots in (b) and (c) correspond to these pulse-like inputs. The trajectories are shown from 1 to 300 ms, bold lines indicate that the fourth local model is active $(\rho_4 > 0.3)$. Note how the cycle in (b) gradually drifts away, due to the effect of the slow unstable eigenvector.



Figure 6. Phase planes of the unstable and the stable local model. The ***** denote the equilibrium points of the autonomous systems, $x_4^e = -A_4^{-1}d_4$. The rectangular area marks the region the local model operates in, cf. figure 5.

local model becomes obvious when a constant frequency burst is applied which drives the model into an operating region where the unstable local model is constantly active. such a response is shown in figure 5(a).

To show how a range of models can fit the data locally, but have quite different properties, we altered the positive eigenvalue to give us a stabilized model with a slow but stable pole at -1. After reidentifying the bias terms d of the modified local model, it performs similarly to the previously identified model on the identification data, cf. figure 4(a), but does not become unbounded for the constant stimulation case. The full force-fields associated with the candidate local models are shown in figure 6.

The above example clearly demonstrates the importance of understanding how a blended multiple model structure represents non-linear dynamics; namely that this understanding can be used to construct a global model with desired properties.

5. Conclusions

In this paper we have made the following important observations regarding the interpretation of local model dynamics in systems of blended local models:

- (1) We have illustrated that a genuine interpretation question arises when the model is identified from experimental data; namely does the identified model represent plant linearizations or global plant dynamics?
- (2) We have shown that the properties (the eigenspace) of the parameterized local models

A(x, u, w) need not provide useful insight into the model dynamics, even in the neighbourhood of model equilibria. The extent to which the local models reflect actual plant dynamics depends on the offsets introduced by linearization points, the form of the interpolation functions, and upon the location of these models with respect to the model equilibria.

(3) We have also demonstrated that a non-unique parameterization of model dynamics exists off equilibria, or when offsets are identified from data. Hence, trying to interpret qualitatively the model dynamics based upon $\mathbf{A}_i(\mathbf{x}, \mathbf{u}, \mathbf{w})$ off-equilibria is dangerous.

The muscle modelling and helicopter examples illustrated that these considerations are relevant for real applications, and that these effects can be used constructively to obtain 'well-behaved' local models. Furthermore, the muscle modelling example also illustrated that the ill-constrained nature of the identified local models can also be a problem, even if the model is used as a black-box structure, i.e. slight variations in identification data can lead to qualitatively different model behaviour. These problems will remain, due to the difficulties associated with experiment design. This can be somewhat constrained by separating the identification of local model offsets and A matrices, so that this case does not occur accidentally for on-equilibrium models. We can also use the non-unique parameterization of the non-linear dynamics to construct global models from local models which are in some sense well

behaved. Future regularization-like approaches could provide a more general solution to apply in the identification stage.

Finally, we emphasize that the interpretation problems reported in this paper arise, not as a result of poor identification, but rather as a result of the nature of the multiple-model approach to building non-linear dynamical models. The authors believe that the full power of this approach will be realized only after the interpretation issue has been understood, and forms an integral part of the experiment design procedure.

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References

- F_{ILLIPOV}, A. F., 1960, Differential equations with discontinuous right hand sides. *Mathematicheskii Sbornick*, **51**, 199–231.
- GOLLEE, H., HUNT, K. J., DONALDSON, N., and JARVIS, J., 1997, Modelling of electrically stimulated muscle. In R.

Murray-Smith and T. A. Johansen (Eds) Multiple Model Approaches to Modelling and Control (London: Taylor and Francis), Ch. 3, pp. 101–120.

- H_{OUSTON}, S., 1994, Validation of a non-linear individual blade rotorcraft flight dynamics model using a perturbation method. *The Aeroneutical Journal*, **98**, 260–266.
- JOHANSEN, T. A., and MURRAY-SMITH, R., 1997, The operating regime approach to non-linear modelling and control. In R. Murray-Smith and T. A. Johansen (Eds) *Multiple Model Approaches to Modelling and Control* (London: Taylor and Francis), Ch. 1, pp. 3-72.
- PRESS, W. H., TEUKOLSKY, S. A., VETTERLING, W. T., and FLANNERY, B. P., 1992, Numerical Recipes (C): The Art of Scientific Computing (Cambridge, UK: Cambridge University Press), 2nd edn, Ch. 15.
- PRIESTLEY, M. B., 1988, Non-linear and Non-stationary Time Series Analysis (Academic Press).
- SHORTEN, R., 1996, A study of hybrid dynamical systems with application to automotive control. PhD thesis, Department of Electrical Engineering, University College Dublin, Republic of Ireland, June.
- SKOOG, R. A., and CLIFFORD, G. Y., 1972, Instability of slowly varying systems. *IEEE Transactions on Automatic Control*, 17, 86-92.
- TAGAKI, T., and SUGENO, M., 1985, Fuzzy identification of systems and its applications for modeling and control. *IEEE Transactions on Systems, Man and Cyberbetics*, 15, 116-132.
- TONG, H., 1990, Non-linear Time Series: A Dynamical System Approach (Oxford, UK: Oxford University Press), Oxford Statistical Science Series 6.